INFERRING RECONNECTION ENERGY RELEASE FROM UV/EUV SIGNATURES IN FLARES

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Outline

- General background (Magnetic reconnection)
- Project outline
- Model
- Results and comparison with observations

Summary

Magnetic Reconnection

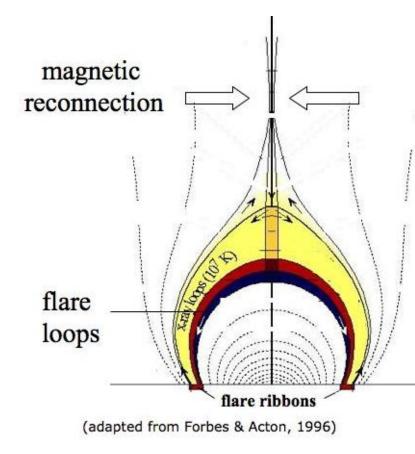
Main phase of flare:

Oppositely directed field lines reconnect

This brings the system to a lower energy state

Energy released -

- heats chromosphere
- forming flare ribbons-observable in UV
- outlines feet of coronal flare loops
- Infer magnetic reconnection rates and energy release rates from time series of flare images



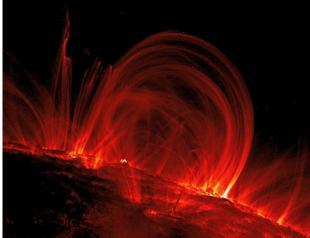
Heat Flux (F_H)

Heat flux - from hot corona to the chromosphere

Initial Stage – F_H > radiation flux (excess heat flux) -drives chromospheric evaporation

- Heated plasma transferred from chromosphere to corona

Later stage - F_H < radiation flux (deficient heat flux) Plasma is drained from coronal loop through cooling – coronal condensation



Project Outline

Aim: Study evolution of flare radiation at foot-points, measure parameters for reconnection and search for a better understanding of the relationship between reconnection and energization of plasmas in flux tubes

- Magnetic reconnection (observe through UV signatures)
- Energy release (heating functions inferred from UV light curve)
- Plasma Evolution (modelled by EBTEL)
- Flare radiation (measured by AIA)
- Modelling radiation output using EBTEL to compare with AIA observations
- Key parameter energy loss through TR (new model)

Measuring Magnetic Reconnection

- Conservation of magnetic flux infer magnetic reconnection flux by measuring magnetic flux present in newly formed flaring regions in the chromosphere
- Measure the reconnection rate:

$$\frac{\partial \phi}{\partial t} = \frac{\partial}{\partial t} (\int \vec{B} \cdot d\vec{a}) \approx \frac{\partial}{\partial t} (\Sigma B_i a_i)$$

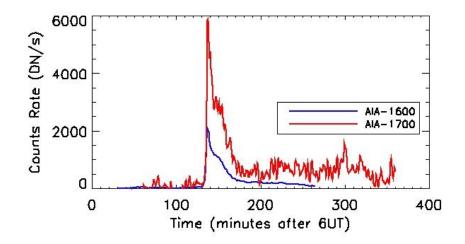
Faraday's Law

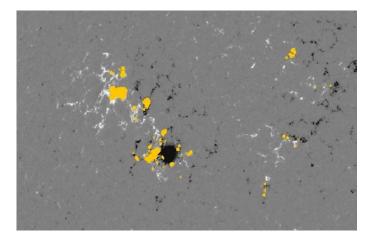
$$\oint \vec{E} \cdot d\vec{l} = -\frac{\partial \phi}{\partial t}$$

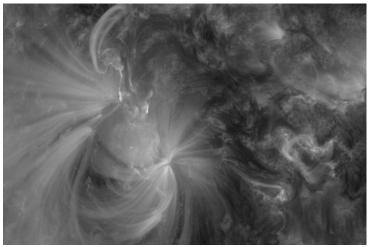
• Energy release rate per unit flux $I(t) = \frac{\int H(t)dt}{\Phi}$

Observations

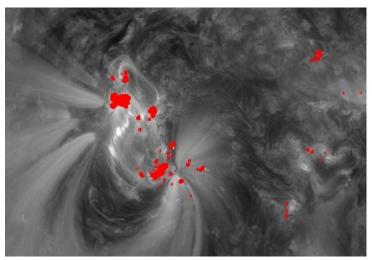
C3.2 flare obtained by AIA/SDO on 1st August 2010







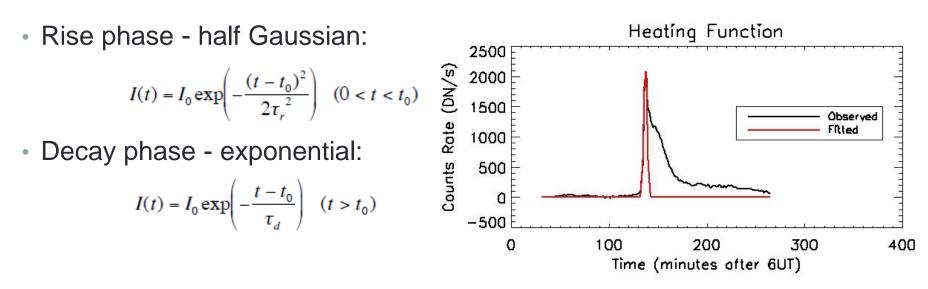




Time: 10:20 UT

Heating Function

• UV light curve of individual pixels reflect timing, amplitude and duration of individual energy release events.



- $H(t)=\lambda I(t)$ where λ is the total heating factor
- Long decay phase cannot be explained by conductive or radiative cooling -> overlying coronal radiation

Measuring Magnetic Reconnection **Reconnection** Flux **Reconnection Rate** 6×10²⁰ (s/xM) 2,0×10¹⁷ Reconnection Flux (Mx) 5×10²⁰ 1,5×10¹⁷ +ve recon rate Rote 4×10²⁰ -ve recon rate +ve recan flux 1.0×10¹⁷ ve recon flux 3×1020 Reconnection 5.0×10¹⁶ 2×10²⁰ 1×10²⁰ ۵ -5.0×10¹⁶ a 50 100 150 200 250 300 0 100 250 50 150 200 0 Time (minutes after 6UT) Time (minutes ofter 6UT) Total recon: $+ve = 7.7 \times 10^{20} \text{ Mx}$, $-ve = -2.6 \times 10^{20} \text{ Mx}$ Total Heating Rate Energy per unit flux histogram tubes) Total heating rate (ergs/s) 4×10²⁸ 3,0 2.5 3×1028 flux 2.0 -DG(Number of 2×10²⁸ 1,5 1.0 1×10²⁸ 0.5 a 0,0 250 0 50 100 150 200 300 2 10 0 6 8 Time (in minutes after 6UT) Energy per unit flux (10-8 A)

Total heating energy = 1.6×10^{30} ergs

EBTEL Model

- OD Enthalpy Based Thermal Evolution Of Loops Model describes average temperature, density and pressure across a coronal strand (Klimchuk et al. 2008 and Cargil et al. 2012)
- Equate enthalpy flux of evaporating and condensing plasma with any excess or deficit in F_H relative to $R_{TR.}$

$$\frac{d\bar{n}}{dt} = -\frac{c_2}{5c_3kL\bar{T}}(F_0 + \mathcal{R}_{\rm tr}), \qquad \stackrel{Q: \text{ volumetric heating rate (erg s-1 cm-3)}}{L: \log half - length (cm)}, \qquad \stackrel{L: loop half - length (cm)}{E_0: \text{ thermal conduction flux (erg s-1 cm-2)}}{R_c: \text{ coronal radiation rate (erg s-1 cm-2)}}, \qquad \stackrel{Q: volumetric heating rate (erg s-1 cm-3)}{R_c: coronal radiation rate (erg s-1 cm-2)}, \qquad \stackrel{R_r: \text{ energy loss rate through transition region (erg s-1 cm-2)}}{R_r: energy loss rate through transition region (erg s-1 cm-2)}.$$

Where $Q = \frac{H}{L}$ and it is assumed that $R_{TR} = c_1 R_c$ where $\mathcal{R}_c \approx \bar{n}^2 \Lambda(\bar{T}) L$

Modification to EBTEL Model

- Unrealistic to scale R_{TR} to $R_{C.}$ Best guess is to scale R_{TR} with pressure.
- Static Equilibrium Case $R_{TR} = \int_{10^4}^{10^6} \Lambda(T) DEM(T) dT$

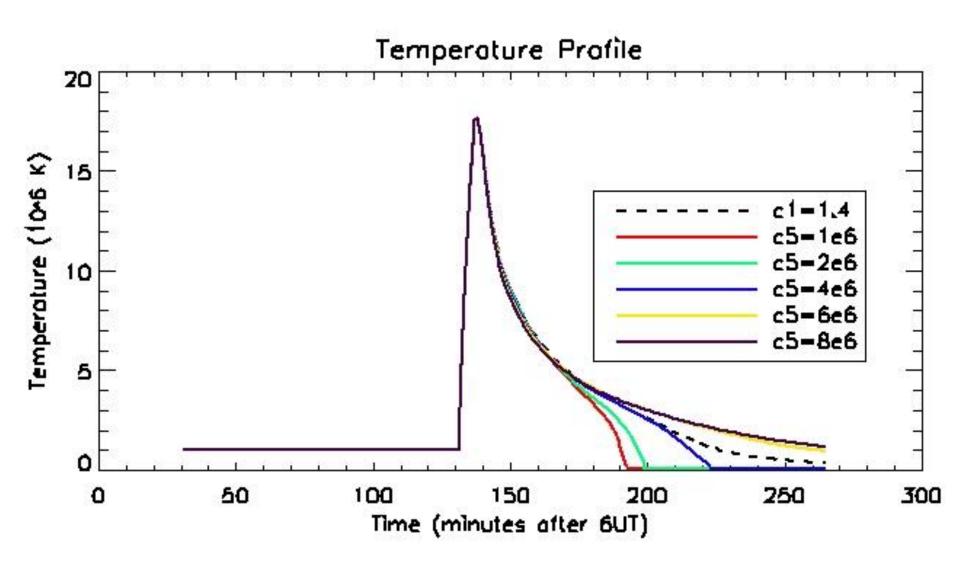
$$DEM(T) = g(T)P$$

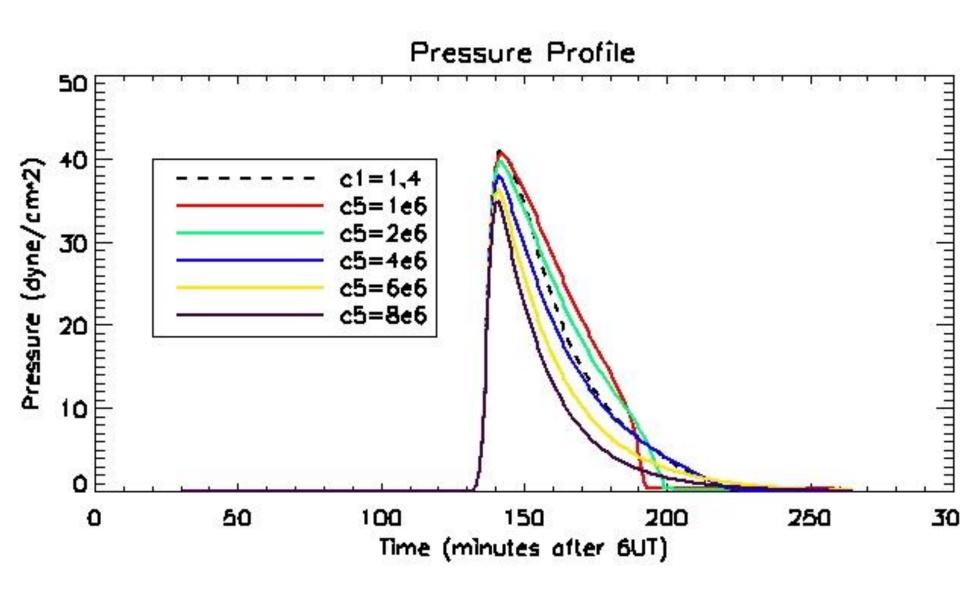
$$g(T) = \sqrt{\frac{\kappa_0}{8k_B^2}} T^{\frac{1}{2}} \left[\int_{T_0}^T T^{\frac{1}{2}} \Lambda(T') dT' \right]^{-\frac{1}{2}}$$

$$R_{TR} = P \int_{10^4}^{10^6} \Lambda(T) g(T) dT C_5$$

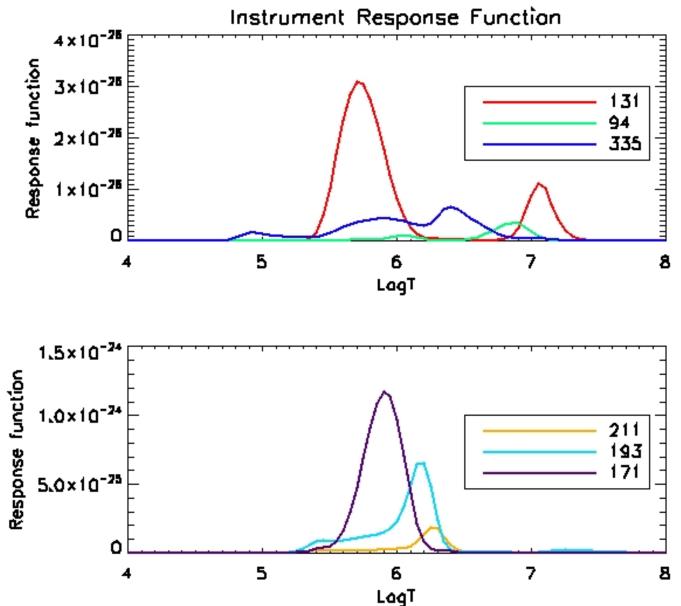
Results

Pressure gauge method $-c_5 = 2 \times 10^6$ Scaling with coronal radiation $-c_5=2.8 \times 10^6$ Density Profile 20 15 Density (10~9/cm·3) c1 = 1.4c5=1e6 c5=2e6 c5=4e6 10 c5=6e6 c5=8e6 5 Ó 0 50 100 150 250 200 300 Time (minutes after 6UT)



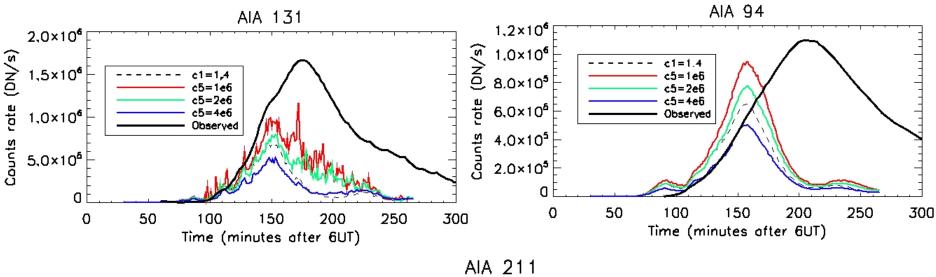


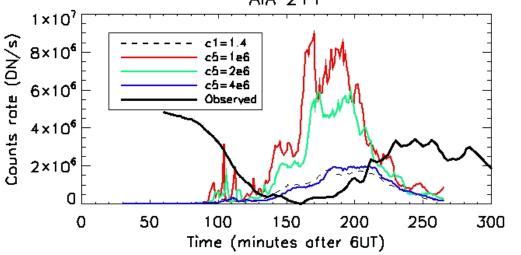
AIA Instrument Response Function



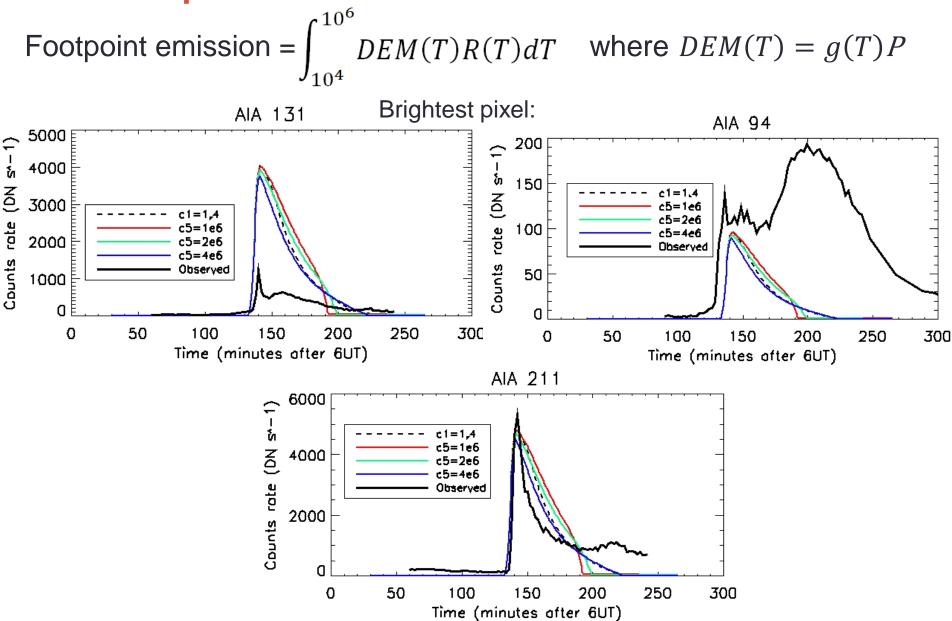
Coronal Observations

Coronal radiation = $\sum_{i} n(T_i)^2 L(T_i) R(T_i)$

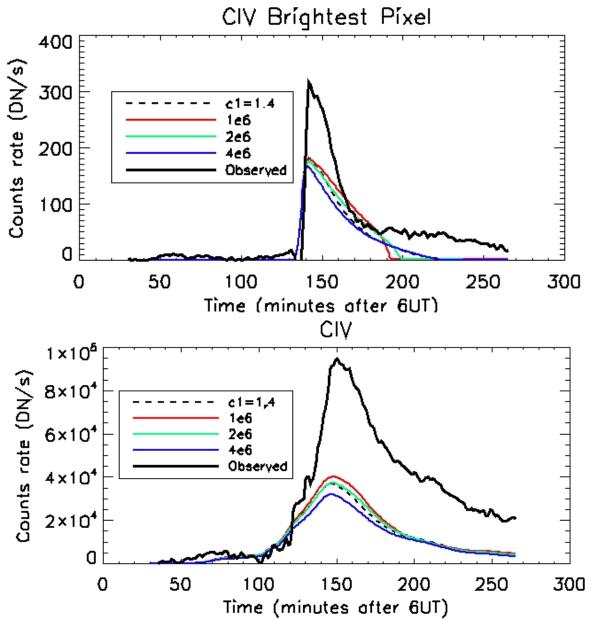




Foot-point Observations



Carbon 4 Comparison



Summary

- UV footpoint emission -> calculate heating rate -> energy release rate
- Total heating energy = 1.6×10^{30} ergs Total reconnection flux = 5.15×10^{20} Mx
- Established connection between reconnection, energy release and loop heating
- Modified EBTEL model $R_{TR} = c_5 P$
- Physically motivated approach
- Early decay slowed down
- In future modify heating function?
- Calculated coronal radiation fits reasonably well in heating phase
- Calculating foot-point radiation using pressure-gauge method fits reasonably well with observations
- In future 1D model connecting foot-point to coronal loop?

Thanks for your attention!